

Evaluation of Co-firing and Reburning Biomass Syngas in a Coal-fired Boiler

B. Adams, H-S Shim

Reaction Engineering International

K-T Wu, H-T Lee, H-P Wan

Energy & Resources Laboratory – ITRI

S-L Chen

Pacific Rim Technologies

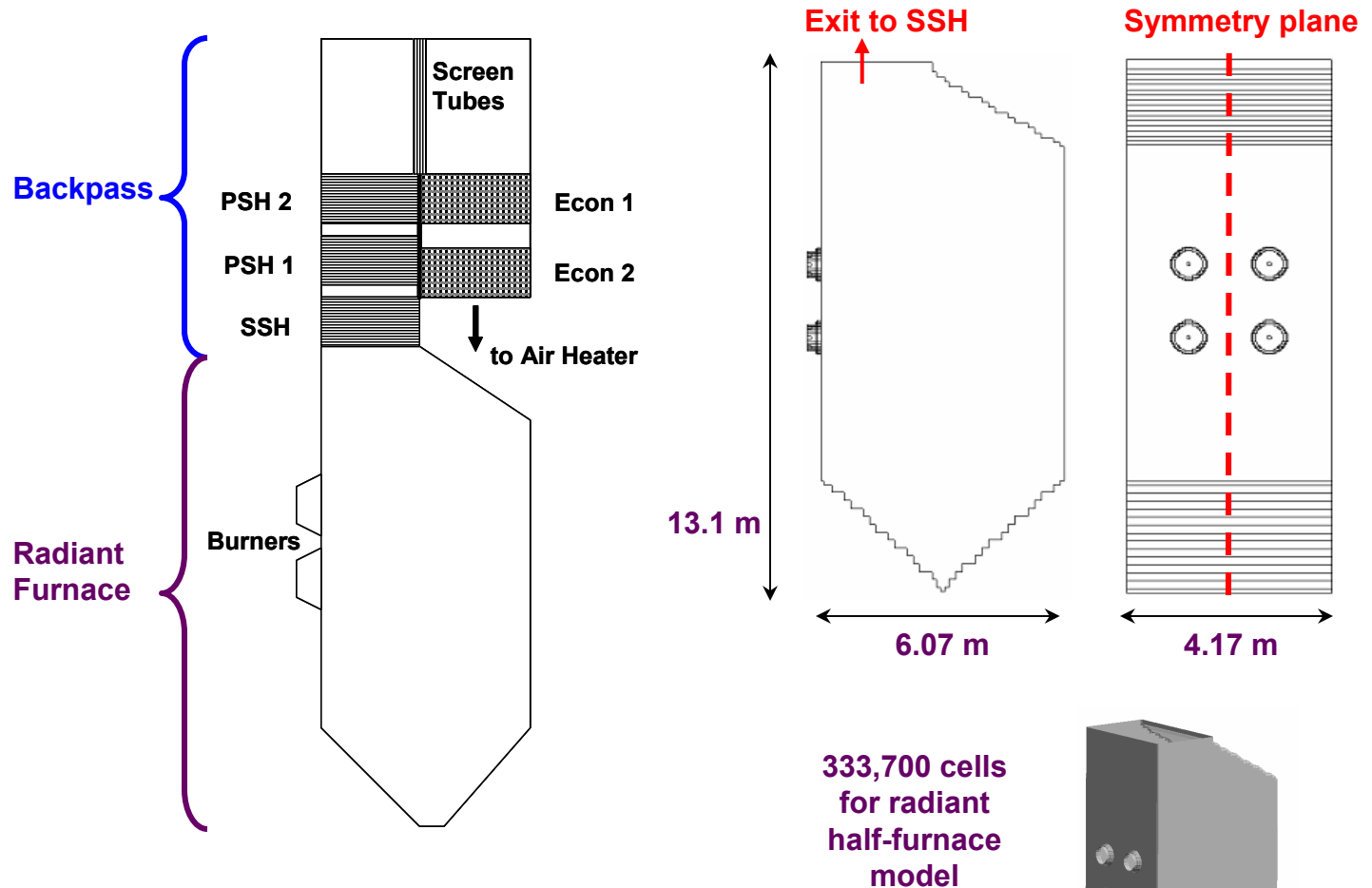
Morgantown, West Virginia

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Project Objectives

- **Evaluate the feasibility of syngas utilization in a coal-fired boiler**
 - Syngas from gasified paper mill rejects
- **Quantify impacts of syngas co-firing and reburning on:**
 - NO_x, CO, LOI
 - Furnace thermal efficiency
 - Corrosion
- **Provide guidance on syngas injector design / boiler operation**

Furnace Design (70 tph steam)



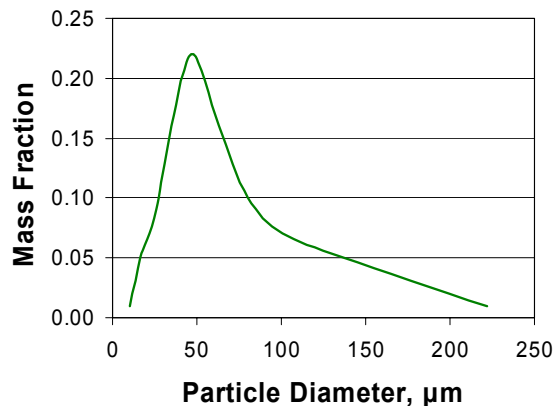
- **Use separate analyses for furnace and backpass**

Fuel Properties

Coal Properties

	Ping Shuo Coal wt%-as rcvd
C	65.59
H	3.95
O	7.96
N	1.2
S	0.26
Ash	12.64
Moisture	8.4
Volatile	25.62
Fixed C	53.34
HHV (BTU/lb)	11453

Particle Size Distribution



Syngas Properties

	Cases 1-4	Case 5
Moisture, %wet	22.78	21.99
N ₂	46.96	49.42
H ₂	7.79	6.86
CO	5.17	4.37
CO ₂	11.64	12.47
CH ₄	3.78	3.43
C ₂ H ₂	0.34	0.33
C ₂ H ₄	1.47	1.01
C ₂ H ₆	0.031	0.023
NH ₃	0.045	0.090
HCN	0.005	0.004
HHV, kcal/kg	1,247	1,085

- Low heating value (NG = 12,872 kcal/kg)
- Low hydrocarbons (~5%), H₂ and CO
- High NH₃ and HCl

Summary of Cases

- **Baseline Simulation**
 - Coal only case
- **Syngas co-firing (Case 1)**
 - 5% heat input through burners
- **Syngas reburning (Cases 2-4)**
 - 10% heat input with fuel-lean reburning configuration ($SR > 1$ above burners)
 - 10% heat input with lowered overall stoichiometric ratio
 - 23% heat input with traditional reburning configuration ($SR < 1$ above burners, overfire air)
- **Syngas composition change (Case 5)**
 - Same operating conditions as Case 3

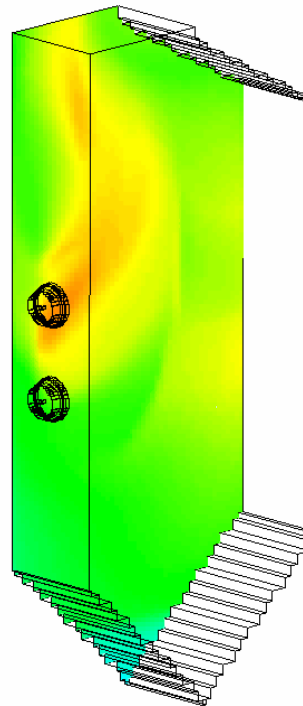
Baseline & Case 1 Inputs

- **Baseline: high swirl burners with no syngas**
- **Case 1: inject syngas at burner centerline**
 - Enhance NH_3 and HCN
 - Add FGR-type dilution effects
 - Need high volume of gas to replace coal
 - Syngas amount limited to 5% by burner size

	Base	case1
Stoichiometric Ratio	1.30	1.30
Exit O₂ %, dry	4.95	4.95
Total Firing Rate, 10⁶ BTU/hr	206.6	206.6
Coal		
Feeding Rate, kg/hr	8,180	7,771
Firing Rate, 10 ⁶ BTU/hr	206.6	196.2
Syngas		
Heat Replacement	NA	5%
Feeding Rate, kg/hr	NA	2,087
Firing Rate, 10 ⁶ BTU/hr		10.3
Primary Air		
% of Total Air	20.0%	20.0%
Temp, °C	75	75
Flow Rate, kg/sec	5.07	4.95
Secondary Air		
% of Total Air	80.0%	80.0%
Temp, °C	260	260
Flow Rate, kg/sec	20.29	19.81
Overfire Air		
% of Total Air	NA	NA
Temp, °C		
Flow Rate, kg/sec		

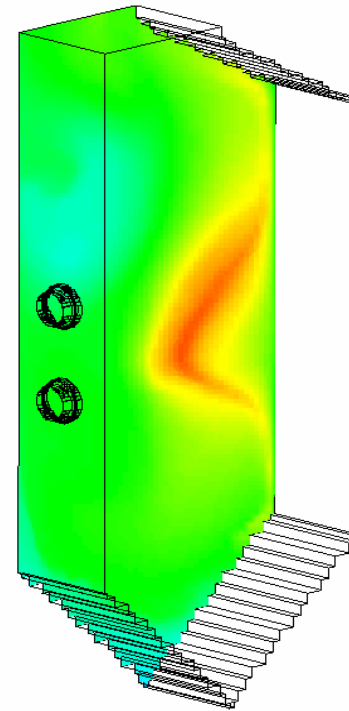
Furnace Temperature: Baseline & Case 1

Baseline

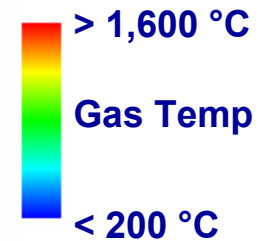


Exit Temp: 1,142 °C

Case 1



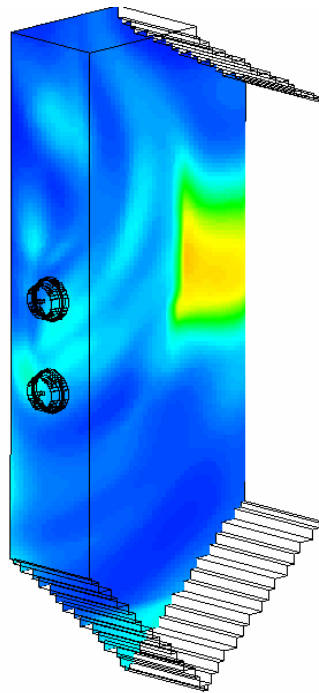
Exit Temp: 1083 °C



- **Case 1 inefficient burner mixing leads to longer flame and lower exit temperature**

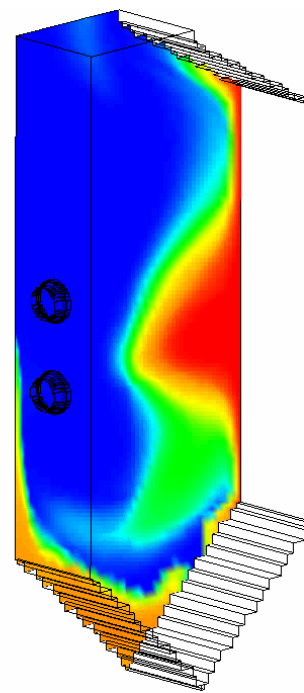
CO Concentration: Baseline & Case 1

Baseline

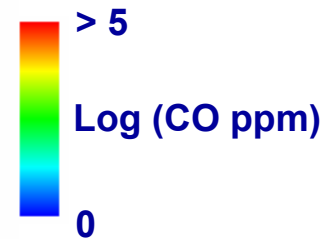


Exit CO: 3,859 ppm

Case 1



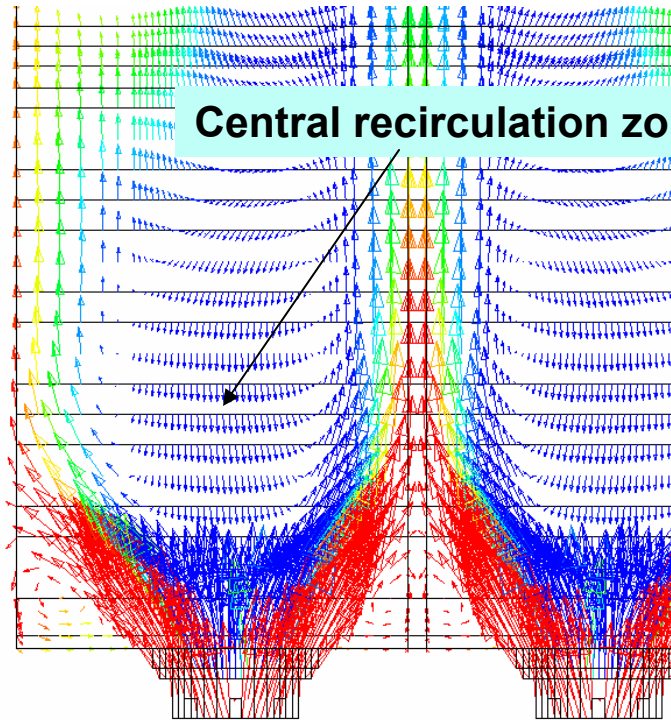
Exit CO: 16,780 ppm



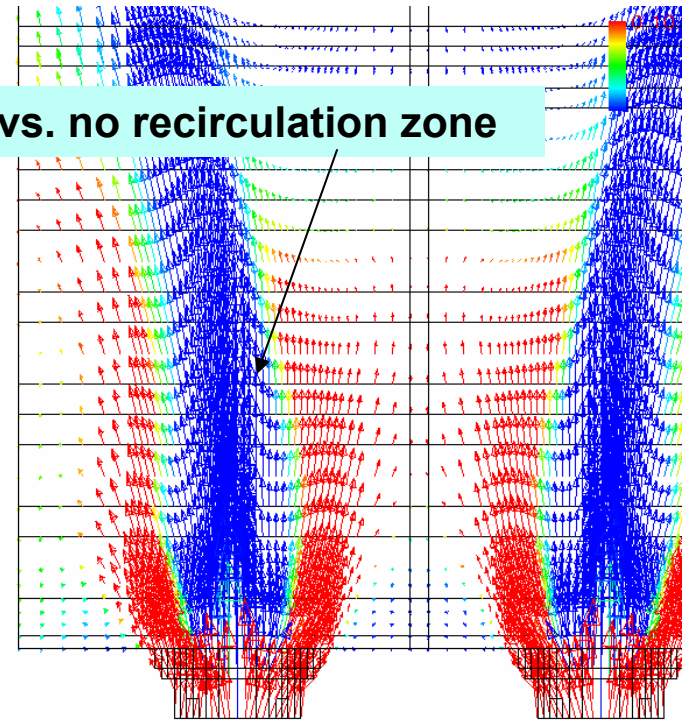
- **Case 1 has much higher CO due to poor mixing**

Burner Flow Patterns: Baseline & Case 1

Baseline Bottom Burner

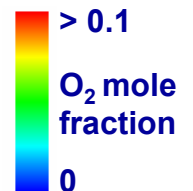


Case 1 Bottom Burner



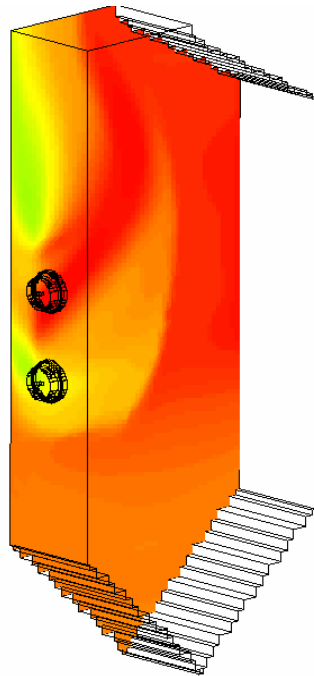
Central recirculation zone vs. no recirculation zone

- High velocity syngas injection eliminates recirculation zone and changes flame shape



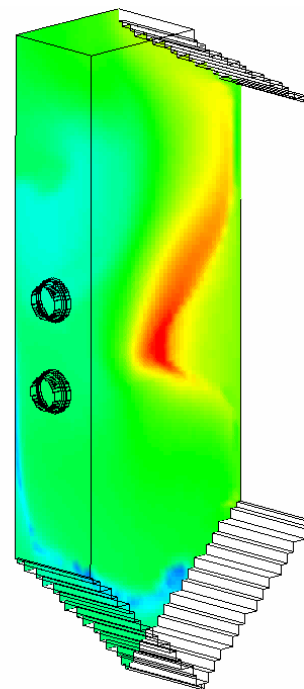
NO_x Concentration: Baseline & Case 1

Baseline

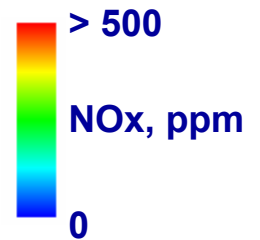


Exit NO_x: 460 ppm
@ 6% O₂ dry

Case 1



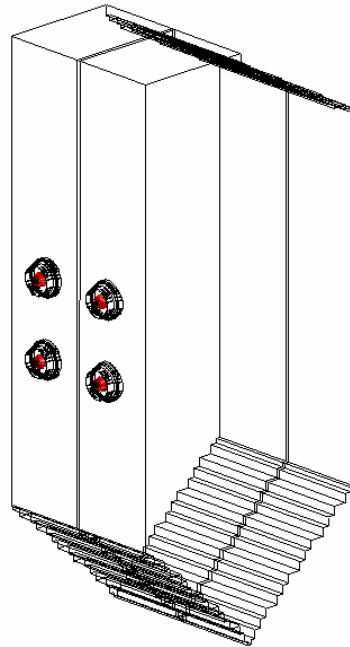
Exit NO_x: 283 ppm
@ 6% O₂ dry



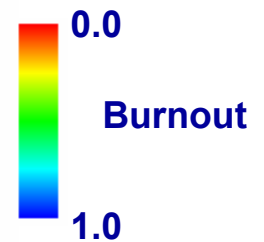
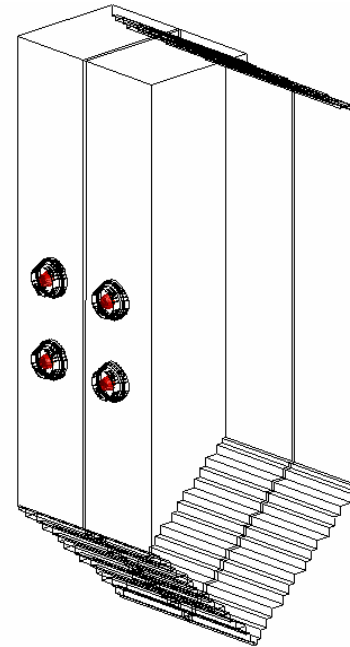
- **Case 1 has much lower NO_x formation due to inefficient mixing**

Particle Burnout: Baseline & Case 1

Baseline



Case 1

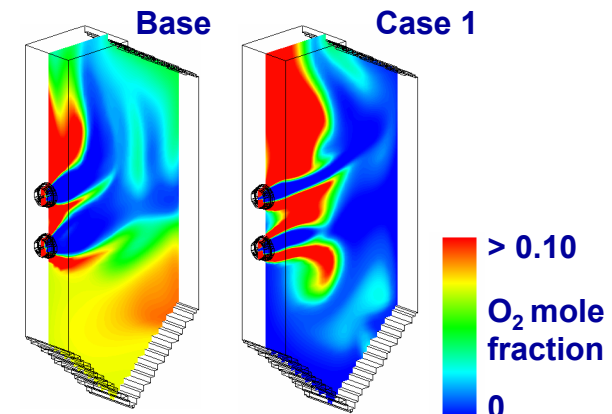


- **Burnout (LOI) depends on: coal reactivity, particle temperature, particle size, oxygen, residence time**
- **Case 1 has more particle deposition on furnace walls**

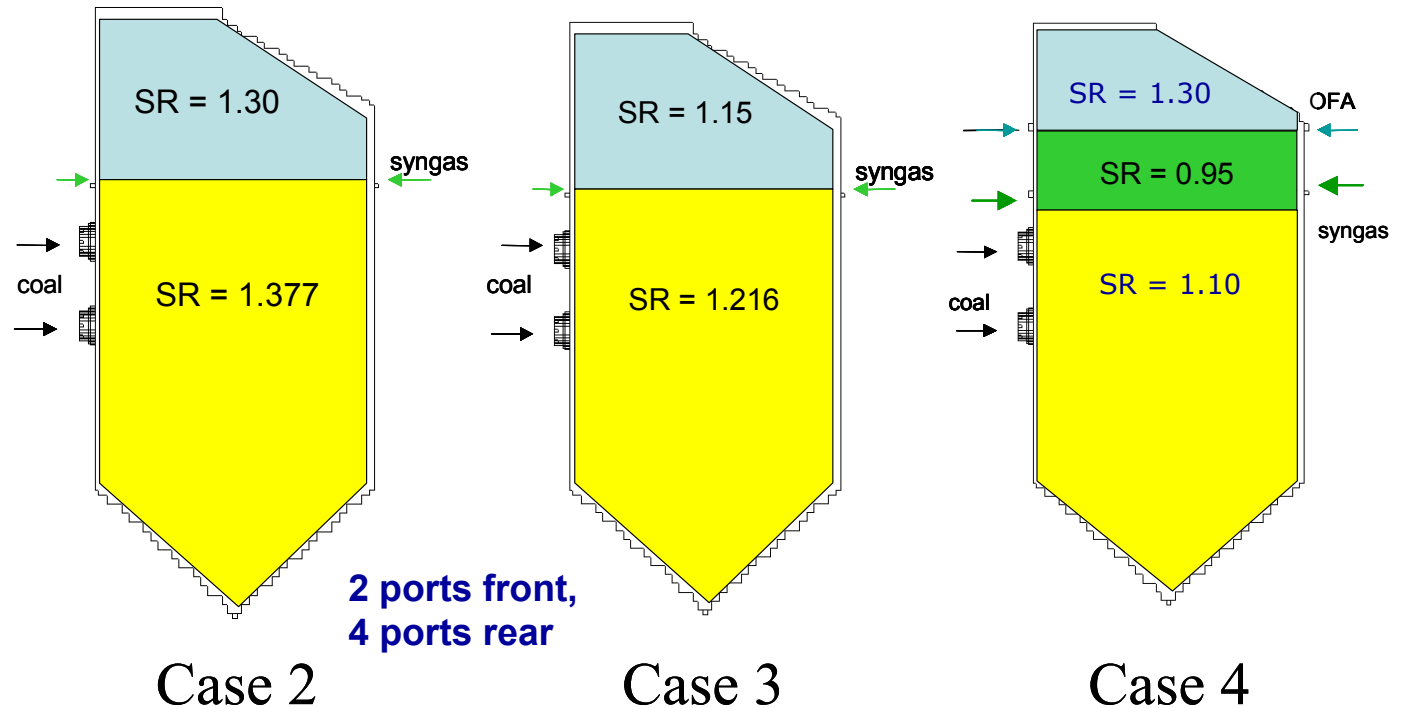
Baseline & Case 1 Summary

- **Baseline has typical high swirl/high NO_x flames**
- **Syngas burner injection collapsed burner recirculation zone & changed flame shape**
 - **Lower NO_x**
 - **Higher CO and LOI (stratified O₂ distribution limits some particles oxygen exposure)**
 - **Flames/particles could impinge rear wall**
- **Case 1 not feasible for good combustion**

RESULTS	Base	case1
Furnace Exit Temp, °C	1,142	1,083
Furnace Exit CO, dry ppm	3,859	16,780
LOI Total, %	6.5	15.0
Upper Burner Row LOI, %	11.1	22.7
Lower Burner Row LOI, %	1	3.8
NO _x , 6% Dry, ppm	460	283
% NO _x Reduction		38



Syngas Reburning

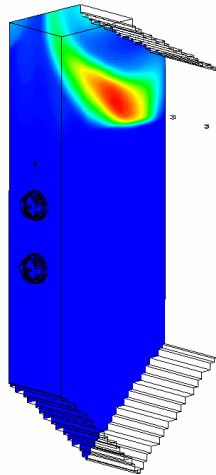


- Use syngas to replace coal and to create fuel rich regions for NO_x reduction (reburning)
- Cases 2&3: lean syngas reburning (LSR)
- Case 4: traditional (overfire air) reburning

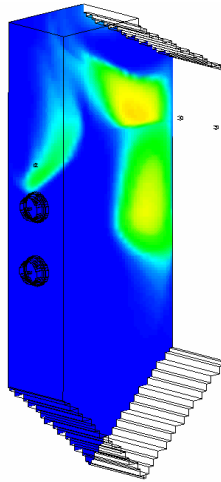
Case 2 Summary

(LSR, 10% syngas, SR=1.30)

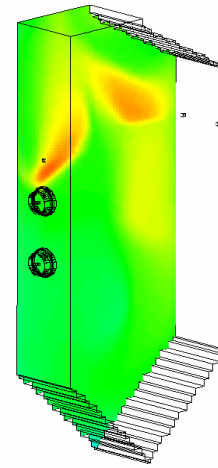
Syngas Fuel



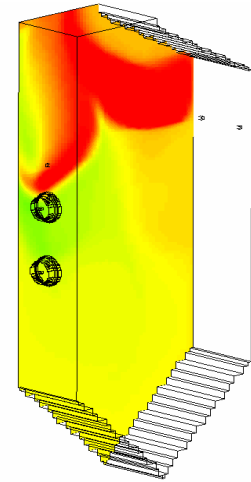
CO



Temperature



NOx

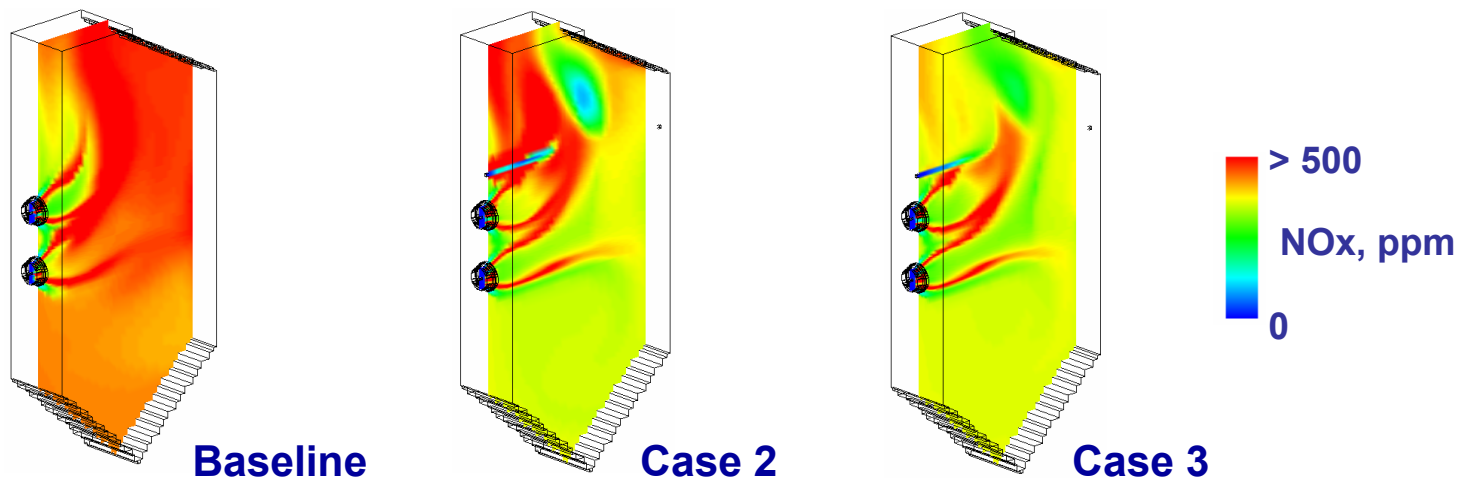


- **NOx reduction in upper furnace balanced by higher NOx formation from burners – net 12% reduction**
- **CO and LOI lower than Baseline due to better mixing and increased burner oxygen**

Case 3 Summary

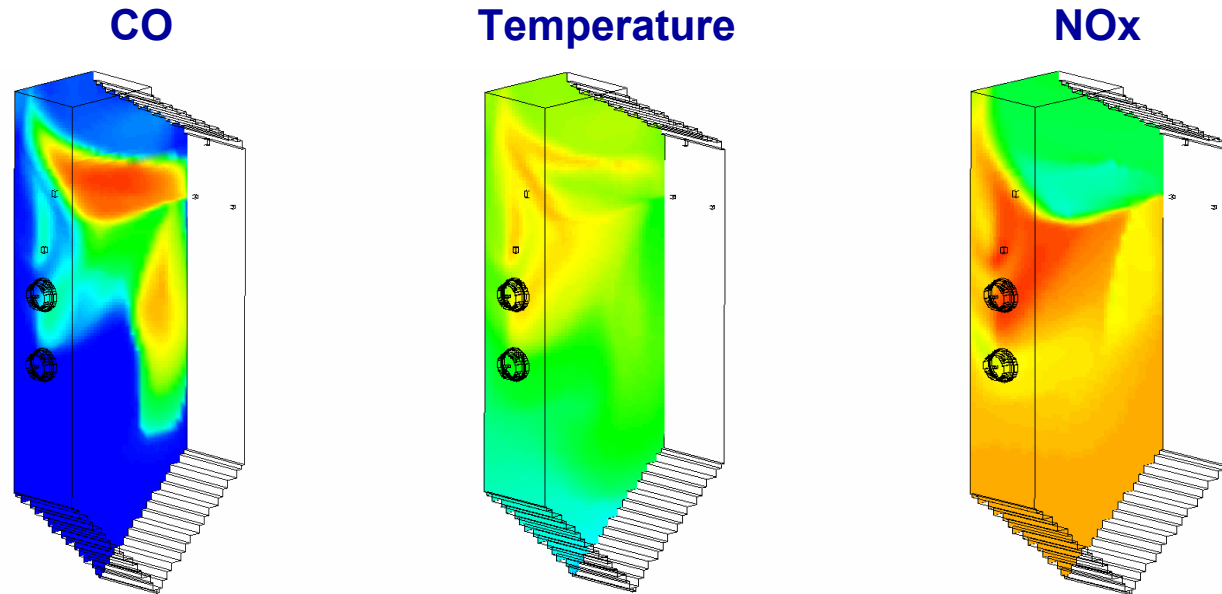
(LSR, 10% syngas, $SR=1.15$)

- Profiles similar to Case 2
- Lower furnace NOx similar to Case 2
- Lower oxygen produced less NOx in upper furnace and allowed more effective reburning
- Net 30% NOx reduction from Baseline
- Lower oxygen increased furnace exit CO and LOI (nearly triple Case 2)



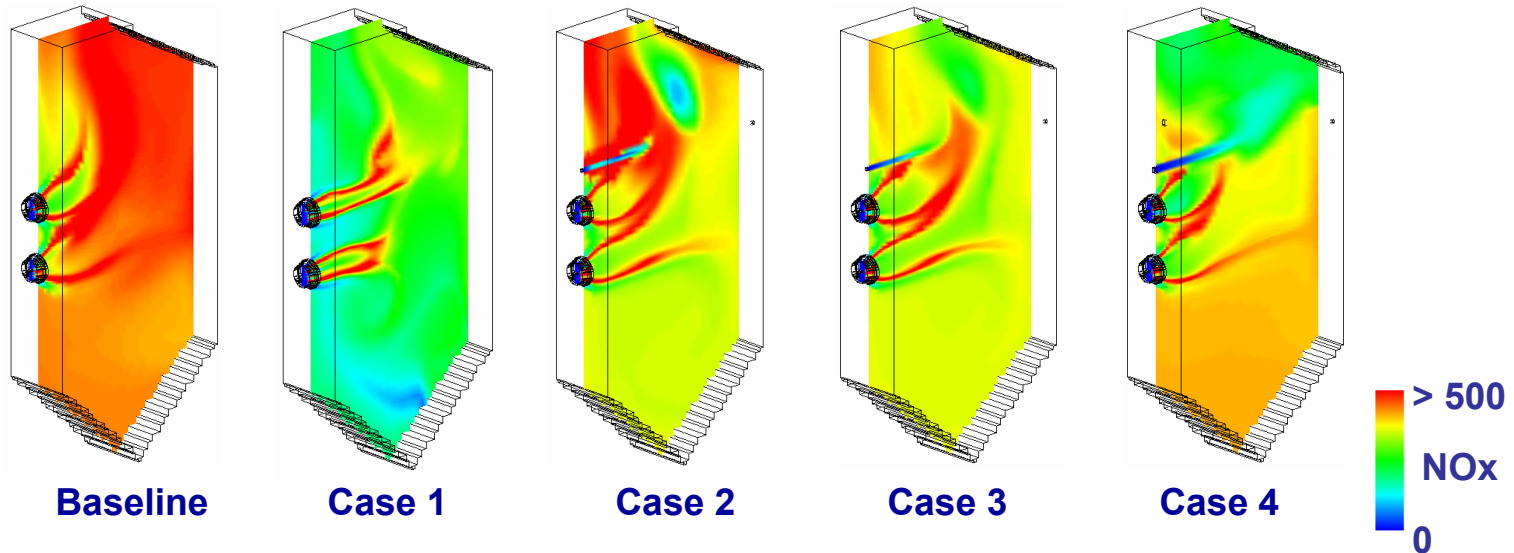
Case 4 Summary

(TR, 23% syngas, 27% OFA, SR=1.30)

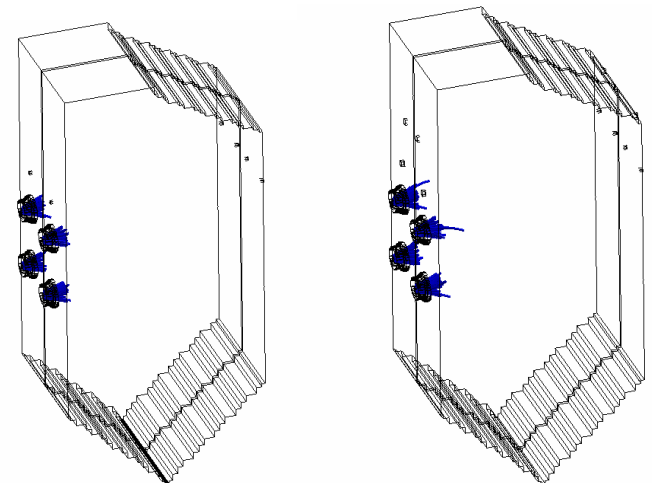


- Increased NOx reduction in reburn zone greater than increased NOx in lower furnace (net 46% reduction)
- Low exit CO due to good OFA mixing
- LOI higher than Baseline and Case 2 due to less oxygen in burner zone and reburn zone

NOx Differences



- **NOx impacted by:**
- Burner mixing
 - Burner stoichiometry
 - Furnace flow patterns
 - Syngas quantity & distribution
 - Furnace geometry



Cases 2-4 Summary

RESULTS	Base	case1	case2	case3	case4
Furnace Exit Temp, °C	1,142	1,083	1,164	1,182	1,201
Furnace Exit CO, dry ppm	3,859	16,780	2,061	6,396	190
LOI, %	6.5	15.0	4.0	11.0	8.6
NOx, 6% Dry, ppm	460	283	406	323	250
% NOx Reduction		38	12	30	46

- **FEGT dependent on heat release elevation and SR change (Case 3)**
- **Exit CO dependent on SR and mixing**
- **LOI dependent on oxygen availability & mixing**
- **Traditional reburning gives best NOx reduction with minimal operational impacts**

Case 5 Summary

(LSR, 10% syngas, SR=1.15)

- **Case 5 has same inputs as Case 3 except syngas composition**
 - **Lower heating value, more NH_3 , less HCl**
- **Case 5 results almost identical to Case 3**
- **Why doesn't higher syngas NH_3 have a greater impact on NO_x ?**
 - **NH_3 concentration from coal flame is higher than from syngas, i.e., coal reactions dominate NO_x formation**
 - **10% syngas heat input is only $\sim 5\%$ of system mass flow \rightarrow small changes in syngas composition do not effect syngas performance**

Summary

- **All reburning designs reduced NO_x, but also produced operational impacts**
- **Lower excess oxygen resulted in lower NO_x for lean syngas reburning**
- **Lowest NO_x with traditional reburning design**
 - **Due to combination of suppressed formation and enhanced reduction above burners**
 - **Higher CH₄ or CO syngas may be difficult to use due to short residence time for CO oxidation**
- **Performance not impacted by changes in syngas composition**
- **NO_x reductions limited by boiler geometry**
- **Reburn design and effectiveness are boiler dependent**

Additional Information

For more information contact REI at

www.reaction-eng.com